

AESB 2320 Physical Transport Phen. Part 2 15 April 2015

1. a) The water is well-mixed, so we can use a macroscopic balance on the reactor in the tank.

$$\text{heat in by convection: } \omega C_p T_{w0}$$

$$\text{"out"} : \omega C_p T$$

$$\text{heat lost through tank bottom: } h A (T - T_c)$$

$$\text{accumulation: } \therefore V_p C_p \frac{dT}{dt} = 0$$

$$\text{energy balance: } \omega C_p (T_{w0} - T) - h A (T - T_c) = V_p C_p \frac{dT}{dt}$$

$$\text{b) At steady state, } \frac{dT}{dt} = 0; \quad \omega C_p (T_{w0} - T) - h A (T - T_c) = 0$$

$$\omega C_p (T_{w0} - T) = h A (T - T_c)$$

$$\omega C_p T_{w0} + h A T_c = h A T + \omega C_p T$$

$$T = \frac{\omega C_p T_{w0} + h A T_c}{\omega C_p + h A}$$

$$2. \text{ a) What is } Re? \quad V = Q/\pi R^2 = \frac{0.05}{\pi (0.05)^2} = 6.37 \text{ m/s}$$

$$Re = \frac{\rho V D}{\mu} = \frac{(0.1)(6.37)(1008)}{0.00059} = 1.088 \cdot 10^6 \quad \text{highly turbulent}$$

$$\text{Eq. 11.3-16 applies} \quad Pr = \frac{C_p \mu}{k} = \frac{(4157)(0.00059)}{0.635} = 3.86$$

$$N_{Re} = 0.026 \quad Re^{0.8} \quad Pr^{1/3} = 0.026 (1.088 \cdot 10^6)^{0.8} (3.86)^{1/3}$$

$$= 2754$$

$$\text{Eq. "III": } N_{Re} = \ln \left(\frac{T_f - T_b}{T_o - T_{b2}} \right) Re Pr \frac{D}{4L} = \ln \left(\frac{30 - 70}{30 - 40} \right) (1.088 \cdot 10^6) 3.86 \frac{0.1}{4 \cdot L}$$

$$2754 = (1.386)(1.05 \cdot 10^5)/L$$

$$L = 52.9 \text{ m} \quad (\text{a little more than 8 sec. travel})$$

b) Now we use the version of the eq. w/o (Δx) :

$$\frac{Q_p D_0}{K} = \ln \left(\frac{T_f - T_{b1}}{T_o - T_{b2}} \right) Re Pr \frac{D_0}{4L} \quad [\text{note } D_0 \text{ cancels on both sides}]$$

$$(Q_p D_0) = \ln \left(\frac{30 - 70}{30 - 40} \right) (1.088 \cdot 10^6) (3.86) \frac{0.1635}{4 \cdot 3000} = 308 \text{ W/m}^2 \text{ K.}$$

$$\text{c) from Eq. (12.6-31), } \frac{1}{R_D D_0} = \left[\frac{1}{\ln h_o} + \frac{\ln (D_{15}/D_{05})}{K} \right]$$

$$\frac{1}{(0.05)(308)} = \frac{1}{(0.05)(3000)} + \frac{\ln 3}{K}$$

$$0.0649 - \frac{1}{3000} = \frac{\ln 3}{K} \rightarrow K = 17.2 \text{ W/m K}$$

$$\text{Q.D.P.S. we need } h_o. \text{ From (a), } N_{Re} = \frac{h D}{K} = 2754 = \frac{h (0.05)(0.1)}{0.0535} \rightarrow h = 27500$$

3. Radiation + convective heat transfer over "in parallel". In this case, Rocky wants a "clean measurement" where all the measured heat transfer reflects radiation. More convection \rightarrow more convective heat transfer, which he would incorrectly ascribe to radiation. In the extreme case, heat transfer might be dominated by convection, giving no information at all on radiation. Therefore he wants to suppress convective heat transfer, by making the air as still as possible.

4. a) It's a solid; no convection.

✓ conduction

✓ generation ("uniform heating")

\Rightarrow accumulation at steady state.

$$b) i) \text{ at } x=0 \quad q_x = 0 \quad \text{or} \quad \frac{dT}{dx} = 0$$

$$ii) \text{ at } x=H \quad q_x = h(T - T_c) \quad \text{or} \quad -k \frac{dT}{dx} = h(T - T_c)$$

(note $q_x > 0$ if solid $T > T_c$)

5. 1. cylinder

$$R=0.05 \text{ m or } D=0.1$$

2. finite-width slab $B=0.2 \text{ m or } D=0.4 \text{ m}$

{ (effective width doubled by insulated surface) }

[No third component]